

トリチウム増殖材データベース (4)
(Li_2O , Li_2TiO_3 , Li_2ZrO_3 and Li_4SiO_4 固体増殖材)

二村 嘉明

富山大学・水素同位体科学研究センター

〒 930-8555 富山市五福 3190 番地

河村 弘*, 土谷 邦彦*

*日本原子力研究所

〒 311-1394 茨城県東茨城郡大洗町成田町新堀 3607

**Tritium Breeding Materials Data Base
for Fusion Reactor Blankets (4)
(Li_2O , Li_2TiO_3 , Li_2ZrO_3 and Li_4SiO_4
Solid Breeding Materials)**

Yoshiaki FUTAMURA

Hydrogen Isotope Research Center, Toyama University

Gofuku 3190, Toyama 930-8555, JAPAN

Hiroshi KAWAMURA* and Kunihiro TSUCHIYA*

*Japan Atomic Energy Research Institute

Shinbori 3607, Narita-cho, Oarai-machi

Higashi-Ibaragi-Gun, Ibaragi 311-1394, JAPAN

(Received December 28, 1999 ; accepted March 31, 2000)

ABSTRACT

This up-to-date compilation of data for ceramic breeding materials (Li_2O , Li_2TiO_3 , Li_2ZrO_3 , and Li_4SiO_4) is part of a study to construct a database for tritium breeding materials of fusion reactor blankets in which existing data for breeding materials and neutron multipliers have been collected from as many

sources as possible.

The data compiled include data on physical and thermal properties, mechanical properties, chemical stability and compatibility, tritium solubility and transport, irradiation effects, afterheat characteristics, thermal cycling effects, waste disposal, and other miscellaneous properties of ceramic breeding materials, such as Li_2O , Li_2TiO_3 , Li_2ZrO_3 , and Li_4SiO_4 . As a result of this compilation, the status of existing data can be recognized.

1. Introduction

Lithium containing ceramics, such as Li_2O , Li_2TiO_3 , Li_2ZrO_3 , and Li_4SiO_4 , are recently considered as promising candidate tritium breeding materials for fusion reactor blankets. Up to this time, authors have endeavored to collect and compile data on many kinds of properties for those materials from as many literature as possible in order to construct a data base for them.

Then, authors rearrange data which have been collected until now, in order to recognize the status of collected data on a variety of properties for candidate breeder ceramics, and to plan the further investigation program for completing the construction of a database.

This compilation of data has made it clear in what properties of some materials there are uncertainties, discrepancies and good agreements. Therefore, it can be recognized what properties for candidate ceramics need more investigation.

This up-to-date compilation is a summary containing the our previous reports and newly collected data after the latest report.³⁾

2. Required characteristics for a solid breeding material

The functions of a solid breeding material are: 1) production of tritium from the neutron/lithium reaction and release of the tritium to purge stream; 2) production of thermal energy and conduction to the blanket coolant; and 3) shielding of neutrons. Thus, in evaluating breeding materials, the tritium retention/release properties are considered as primary parameters and the highest of the three. Particularly, solid breeding materials must efficiently perform these functions under high level of neutron exposure and high temperature conditions with maintaining their integrity during operation. Therefore, main required functions and characteristics for solid breeding materials are listed in Table 2-1. For the purpose of helping the evaluation of breeding materials, examples of breeding materials and operating conditions for a fusion reactor blanket are shown in Table 2-2.

Table 2-1 Main required functions and characteristics for solid breeding materials

Function	Required characteristics
Good tritium production, and Breeding characteristics	High lithium content Efficient release/recovery of produced tritium
Proper breeder temperature Control	High thermal conductivity
Good integrity	Good neutron irradiation resistance High mechanical strength, and high durability Good chemical stability Good compatibility with other materials
High safety	Low activation Low reactive with coolant
Fabrication	Mass production at a low price Easy treatment

Table 2-2 Major operating conditions of breeding materials of a fusion reactor.

	ITER	SSTR
Breeding material	Li ₂ ZrO ₃	Li ₂ O
Li burn-up (%)	~5	10~30
Nuclear heat generation (MW/m ³)	~50	~90
Temperature range (°C)	300~750	450~950
Structural material	SS316 LV-IG	RAF(F82H)
Multiplier material	Be	Be
Environmental gas	He gas (~0.1MPa)	He gas (~0.1MPa)

ITER: International Thermonuclear Experimental Reactor.

SSTR: Steady State Tokamak Reactor.

3. Data for solid breeder materials

Up-to-date available data for the solid breeder materials are summarized in Table A-1, A-2, A-3, A-4. These tables are organized by material property in terms of physical properties, thermal properties, mechanical properties, chemical stability/compatibility/interaction with blanket coolant, purge gas, neutron multiplier and structural materials, tritium solubility/transport, irradiation effects, thermal cycle effects, and so on.

Representative properties of candidate breeder ceramics under the specified theoretical density (TD), porosity, and temperature, are summarized in Table 3-1. With numerical values of properties in Table 3-1, the evaluation on which candidate ceramic is considered to be superior to another ceramics, can be easily performed.

Moreover, the present status of breeder material database is shown in Table 3-2, in order to recognize the extent and degree of investigated data on properties for breeder materials.

4. Review of database on properties for candidate breeder ceramics

With regard to a variety of properties of breeder ceramics, the present status of an

existing database for candidate breeder ceramics, such as Li_2O , Li_2TiO_3 , Li_2ZrO_3 , and Li_4SiO_4 , was shown in Table 3-2.

4.1 Physical and thermal properties

In tritium breeding ratio (TBR), Li_2O is considered the only ceramic candidate among Li_2TiO_3 , Li_2ZrO_3 , and Li_4SiO_4 for achieving a TBR larger than unity in the absence of a neutron multiplier.

As for the vapor pressure data, more investigation is required in order to develop a reliable database for breeder ceramics.

4.2 Mechanical properties

The thermal cycling behavior of pebbles 1 mm in size was investigated for Li_2O (92%TD, 42 μm grain size), Li_2ZrO_3 (80%TD, 40 μm grain size), and Li_4SiO_4 (93%TD, 40 μm grain size) under the representative conditions in ITER, i.e. 400-800°C and the heating-cooling rates of 20°C/s (72,000K/h) up to 2000 cycles.⁶⁸⁾ While the Li_2O pebbles performed extremely well, the Li_2ZrO_3 and Li_4SiO_4 pebbles fractured significantly. In contrast, Li_4SiO_4 pebbles 0.4-0.6 mm in size cycled for 50 cycles, showed good behavior. Moreover the thermal cycling behavior of pebbles 1.2 mm in size for Li_2TiO_3 was investigated under 273-1273K at 200 K/h ramp temperature change. The results were summarized in Table 4-1.⁶³⁾

Table 4-1 Effects of thermal cycling on strength of Li_2TiO_3 pebbles

Sample	Strength	Number of thermal cycles					
		0	3	6	9	12	15
77.6% TD 4~10 μm grain	Compressive Strength (N)	40.9	44.9	43.1	42.7	42.3	42.7
81.3% TD 40~140 μm grain	Compressive Strength (N)	35.6	4.4	9.8	33.4	32.5	31.1

The thermal cycling behavior of Li_2ZrO_3 pellets (76.8%TD and 83.5%TD, 8mm length), cycled in the temperature range of 330~550°C, performed well. No fracture was observed after 1000 cycles at an equivalent tangential tensile stress of 30 MPa; 14% fracture was observed for the pellets with 76.8%TD after 10000 additional cycles at 40 MPa. No fracture was observed for the pellets with 83.5% TD Li_2ZrO_3 after 30000 cycles at 47 MPa. The higher the density is, the better is the behavior. Li_2TiO_3 pellets thermal cycling test is in progress. From the first results, Li_2TiO_3 pellets behavior is expected to be similar to that of Li_2ZrO_3 pellets. For the effects of thermal cycling behavior of Li_2TiO_3 , Li_2ZrO_3 , and Li_4SiO_4 more data are needed.

4.3 Chemical stability and compatibility (Interaction with other blanket materials)

In laboratory tests, the interaction of beryllium with Li_2ZrO_3 and Li_4SiO_4 was found to be negligible up to 650°C .⁶⁸⁾ Interaction of Li_2TiO_3 with steels is less than that of Li_2ZrO_3 .

The irradiation effect on the interaction of beryllium and lithium ceramics was investigated. No irradiation effect was detected under the conditions explored at ^6Li burn-up of 20%-40% for natural ^6Li isotope content (Li burn-up of 1.5%-3%).⁶⁸⁾

Lithium contained in Li_2ZrO_3 sintered compacts immersed in water, is slowly but completely dissolved within one month, whereas no dissolution of lithium contained in Li_2TiO_3 sintered compacts is detectable after a 40 days immersion. Also, no uptake of moisture from room air after 6 months exposure is reported on Li_2TiO_3 . Both ceramics are easily soluble in hydrochloric acid.

The tritium solubility data for $\text{Li}_2\text{O}/\text{H}_2\text{O}$ are quite good, but the solubility data for $\text{Li}_2\text{O}/\text{H}_2$ system are quite scattered (factor of 15 spread in the data). The desorption/decomposition data for moisture release from LiOH and Li_2O have a factor of 10 scatter. Adsorption for $\text{Li}_2\text{O}/\text{H}_2$ and $\text{Li}_2\text{O}/\text{H}_2\text{O}$ system needs to be more reasonably characterized. Solubility/adsorption/desorption mechanisms are only poorly characterized for Li_2ZrO_3 , Li_4SiO_4 and Li_2TiO_3 ceramics.

4.4 Irradiation effects

(1) Irradiation behavior

Under conditions of temperature levels of 500, 700, 900°C and up to 3% lithium burn-up, Li_2ZrO_3 showed that swelling was low, physical integrity was excellent, no change of grain size was observed, and tritium and helium retention was very low. On the contrary, Li_2O did high swelling at 3 % burn-up.

After irradiation to 3% burn-up, there was a significant reduction in the thermal conductivity of Li_2O at low temperatures, i.e. under 400°C . At higher temperatures, thermal conductivity values were unchanged or were even higher than the unirradiated values.⁶⁸⁾

No testing of irradiation behavior of Li_2TiO_3 ceramic was almost made to date, except for a few tests of tritium and helium retention, and tritium release. However, the authors suppose that the behavior will be similar to that of Li_2ZrO_3 from our view of reference materials.

(2) Tritium release

For safety and economical reasons the tritium release rate must be enough large that the tritium inventory in the blanket does not become excessive. Tritium residence time (τ) defined as the average time a triton spends in the breeder between generation and release, can be used to relate the tritium inventory to the tritium generation rate.

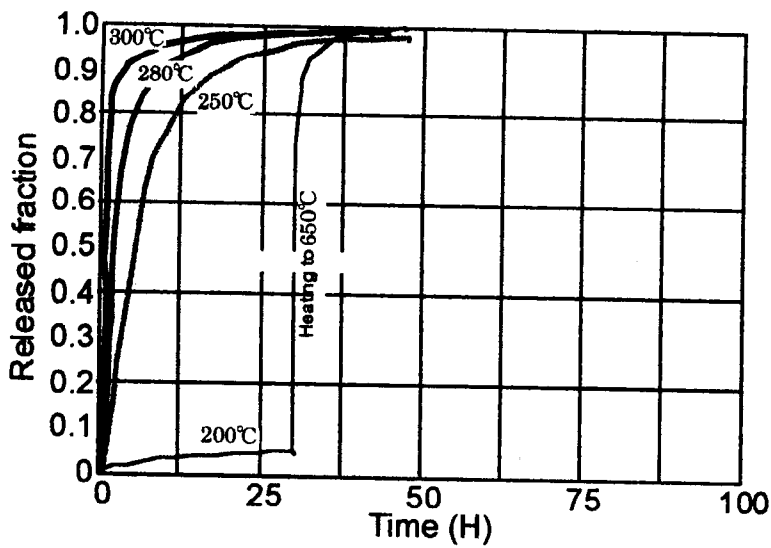


Fig. 4-1 Isothermal tritium release at 300°C, 280°C, 250°C, 200°C, in He + 0.1% H_2 purge gas, flow rate 2.4 l/h for Li_2TiO_3

Tritium residence times were investigated for Li_2O , Li_2ZrO_3 ⁶⁾, and Li_4SiO_4 ⁶⁸⁾ at various temperatures.

The effects of lithium burn-up on tritium release for Li_2ZrO_3 was studied at 4.5%, 7.6% and 9.5% lithium burn-up. Those results reveal no decrease in the tritium release. For the comparison of the tritium release behavior of Li_2ZrO_3 and Li_2TiO_3 up to 9.5% lithium burn-up,

examples of test results are shown in Figs.4-1 and 4-2. These results indicate that those behave similarly. For Li_2ZrO_3 a good tritium release is observed down to 200°C, i.e., 40% tritium released within about 120h. For Li_2TiO_3 a larger decrease in the tritium release between 250°C and 200°C is observed. This difference in behavior with Li_2ZrO_3 reflects the difference in the shape of the tritium release peaks in the linear heating run i.e., sharper peak for Li_2TiO_3 than for Li_2ZrO_3 .

As the estimated minimum temperature for which the residence time is one day, is desirable to be lower from a design viewpoint, the tritium release performance of Li_2ZrO_3 and Li_2TiO_3 are superior to Li_2O and Li_4SiO_4 . Because Li_2O and Li_4SiO_4 are not

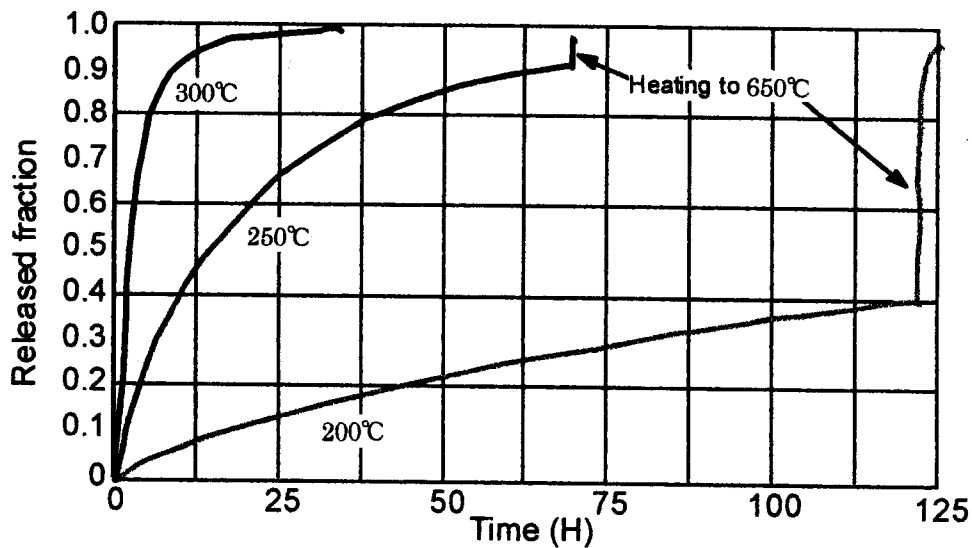


Fig. 4-2 Isothermal tritium release at 300°C, 250°C, 200°C, in He + 0.1% H_2 purge gas, flow rate 2.4 l/h for Li_2ZrO_3

releasing tritium at low enough temperature and/or are too reactive with water.

Therefore, more data are needed for tritium retention and release of Li_2TiO_3 , and more data for helium retention and release are also needed.

(3) Waste disposal

With respect to waste disposal, one must consider the production of long-life radionuclides. For the ceramics, the radioactivity after 1 year is very low in comparison with that of the structural materials. In all cases, activation of the structural materials is higher than that of ceramic breeding materials. The long-life radionuclides, such as ^{94}Nb ($L_{1/2}=2 \times 10^4 \text{y}$), are decay products from Li_4SiO_4 , Li_2ZrO_3 and Li_2TiO_3 . Li_2O does not present a problem for waste disposal. With no impurities, the U.S. Class C waste disposal rating for Li_2TiO_3 is roughly equal to that for Li_2O and Li_4SiO_4 and more than 10 times lower than Li_2ZrO_3 .

Afterheat levels in Li_2TiO_3 are 20~50 times more than in Li_2O and Li_4SiO_4 , but 2~100 times lower than Li_2ZrO_3 .

5. Concluding Remarks

Authors have compiled the up-to-date data for candidate blanket solid breeding materials which have been collected by this time, and somewhat assessed these data. There are less data for Li_2TiO_3 than those for Li_2O , Li_2ZrO_3 and Li_4SiO_4 , since Li_2TiO_3 is recently considered as an attractive candidate breeding material.

As a whole, physical properties and thermal properties are fairly good investigated, but the investigations are not enough. More investigations on fracture strength, specially, tensile strength for breeder ceramics, are required. Data on thermal creep for Li_2TiO_3 are required.

With regard to compatibility, the data on hydrogen solubility and adsorption for Li_2ZrO_3 , Li_4SiO_4 and Li_2TiO_3 are needed. Also the data on water vapor solubility and adsorption for Li_2ZrO_3 , Li_4SiO_4 and Li_2TiO_3 are needed.

For lack of enough data on irradiation effects for breeder ceramics, it is hereafter more needed to investigate irradiation behaviors on physical properties, thermal properties, mechanical properties, tritium transport, retention and release properties, helium transport, retention and release properties, fracture properties, and so on. In this case, Table 3-2 will be helpful for investigators. The more information on tritium release and thermal cycling behavior for Li_2TiO_3 is needed.

However, owing to the limitation of our research and search activity, there may be still oversight of existing data. So the authors are very much grateful for being notified existing data as well as being assisted for collecting the data and/or supplied with them. Only with such collaboration, we can construct the complete database on breeding blanket materials.

Acknowledgement: The authors wish to thank Professor and Dr. K. Watanabe for his continuous and helpful advice.

Table 3-1 Summary of candidate ceramic breeder characteristics.

Property	Li ₂ O	β Li ₂ TiO ₃	Li ₂ ZrO ₃	α Li ₄ SiO ₄
Density, 100%TD, g/cm ³	2.03	3.43	4.16	2.40
Lithium density, g/cm ³	0.94	0.43	0.38	0.55
Phase change temp. °C	370	1150	1100	660
Melting point. °C	1432 ± 6	1535	1695 ± 15	1255
Thermal conductivity W/m.K, 500°C, @ 85%TD Unirradiated	4.4	1.8	1.9	0.9
Thermal expansion, @ RT-700°C, % 600°C 1/K	1.9 26x10 ⁻⁶	1.2 21 x10 ⁻⁶	0.7 9.96 x10 ⁻⁶	1.8 24 x10 ⁻⁶
Thermal diffusivity At 600°C, mm ² /s	0.85	0.55	0.357	0.300
Young's modulus, GPa RT, & 600°C	70.0 & 60.7	123(300K, 80%TD, 1~2 μ m)	89.0 & 77.3	56.3 & 48.2
Poisson's ratio, RT, & 600°C	0.19 & 0.19	0.24(300K, 80%TD)	0.2 & 0.2	0.24 & 0.24
Bending strength, MPa @RT, 85%TD, 10 μ m grains	60	60	60	50
Compressive strength, MPa, RT & 600°C	(65.8) & (28.4)	--	145 & (---)	253 & (--)
Temperature for 0.1 Pa Li Vapor pressure, °C	1120	~ 1300	1300	1210
1- D TRR (optimum % ⁶ Li)	1.46(20)	1.32(51)	1.38(58)	1.34(33)
Creep rate, μ m/m-s (800 °C, 20 MPa)	4.0	--	(≪ 2)	0.184
Swelling, vol, % @ 700°C, 2 at%Li burnup	7.5	--	0.5	1.2
Tritium residence time, hr @ 400°C, 80%TD, 1 μ m grains	1	< 1	< 1	14
Class C waste disposal Rating, @ 15MW.yr/m ² , 10 yr cooling	0.2	0.17	24	0.14
Afterheat, W/cm ³ @ 1hr, 15 MW.yr/m ² , 85%TD	0.001* 10 ⁻⁹ **	0.05 *	6 * 0.05 **	0.003 * 0.0001 **
Steel reaction layer, μ m @ 500°C, 10 ⁴ hr, 10 Pa H ₂ O	8 - 50	< 7	7	20
Be reaction layer, μ m @ 700°C, 10 ⁴ hr, 10 Pa H ₂ O	~200	--	~50 - 100	200 - 600

- Note: 1. Properties of Young's modulus, Poisson's ratio, compressive strength and creep rate, at 80 % TD, 10 μ m grain diameter and 90 % Li-6 enrichment.
2. Values in parentheses are estimated or extrapolated well beyond the data base.
3. * From FINESSE 1987(p.2-125); no impurities; tritium retained in breeder.
4. ** From UKAEA 1989; 12.5 MW.yr/m², no impurities or tritium.

Table 3-2 Data Base Assessment for Solid Breeders (Breeder Ceramics)

	Li ₂ O	Li ₂ TiO ₃	Li ₂ ZrO ₃	Li ₄ SiO ₄
Physical and thermal properties				
Density	■	■	■	■
Melting point	■	■	●	▲
Vapor pressure	▲	○	○	○
Thermal expansion	■	▲	▲	▲
Thermal conductivity	▲	▲	▲	
Specific heat	■	▲	▲	■
Mechanical properties				
Young's modulus	▲	▲	▲	▲
Poisson's ratio	▲	▲	○	▲
Fracture strength				
tensile				
compressive	○	○	○	○
bending	○	○	▲	▲
Creep properties	▲		○	▲
Chemical stability/compatibility				
Composition/purity	■	■	■	■
Stability	■	■	■	■
Vapor pressure/transport	■	○	○	○
Compatibility				
water	▲	■	■	▲
beryllium			▲	■
Stainless Steel	○	▲	▲	■
Tritium solubility/transport				
Tritium solubility	●			
Tritium diffusivity	■		○	○
Adsorption/desorption	●			
Radiation effects				
Physical properties	○		○	○
Swelling	○		○	○
Creep				
Tritium trapping/transport	●	○	○	○
Helium trapping/transport	○	○	○	○
Fracture properties	○	○	○	

- Note: 1. ■ ----- Adequate data base and good agreement
2. ▲ ----- Limited data base and general agreement
3. ● ----- Limited data base and important discrepancies (new data sets have become available)
4. ○ ----- Single set of limited is available.
(More investigations are required)
5. Blank ----- Very limited/non-existent/high uncertainties
(More investigations are required)

Table A-1 Physical and thermal properties of candidate breeder materials

1. Li_2O

1.1 Physical properties

Item	Data	Refs.
Molecular weight, g/g-mol	$30.0314 - 2.002 \delta$, $\delta =$ atom fraction ${}^6\text{Li}$ in Li	9
Crystalline structure	Cubic	9
Density, g/cm ³	$2.0338 (1 - 0.06665 \delta)$	10
Li density, g/cm ³	0.815δ for ${}^6\text{Li}$, $0.950(1 - \delta)$ for ${}^7\text{Li}$,	10
Melting point, °C	1432 ± 6	9

1.2 Thermal properties

Item	Data	Refs.
Vapor pressure, Pa	$\log P(\text{Li}) = - (18.19 \times 10^3 / T) + 12.09$ $\log P(\text{LiO}) = - (19.85 \times 10^3 / T) + 11.21$ $\log P(\text{Li}_2\text{O}) = - (20.60 \times 10^3 / T) + 13.40$ $1532 \leq T \leq 1073 \text{ K}$	11
Specific heat, kJ / kg-K	$C_p = 2.5179 + 3.328 \times 10^{-4} T - 8.382 \times 10^{-7} T^2$ $306 \leq T \leq 1073 \text{ K}$	10
Thermal conductivity, W/m-K	$\kappa = (1 - p)^{1.96} [39.79 (1 + 7.067 \times 10^{-3} T)^{-1}]$ $0.066 \leq p(\text{porosity}) \leq 0.292$, $473 \leq T \leq 1173 \text{ K}$	12
Thermal expansion Linear expansion, % Instantaneous coef. 1/K Mean coef. 1/K	$\Delta L/L_0 = 1.87 \times 10^{-3} (1 + 4.49 \times 10^{-4} T)(T - 298)$ $\alpha = 1.605 \times 10^{-6} (1 + 1.072 \times 10^{-3} T)$ $\alpha_m = 1.87 \times 10^{-5} (1 + 4.49 \times 10^{-4} T)$ $298 \leq T \leq 1223 \text{ K}$	10

2. $\beta\text{Li}_2\text{TiO}_3$

2.1 Physical properties

Item	Data	Refs.
Molecular weight, g/g-mol	$109.93 (1 - 1.82 \times 10^{-2} \delta)$, $\delta =$ ${}^6\text{Li}$ fraction in Li	9
Crystalline structure	Monoclinic	9
Density, g / cm ³	$3.44 (1 - 1.82 \times 10^{-2} \delta)$	9
Li density, g / cm ³	0.37δ for ${}^6\text{Li}$, $0.44(1 - \delta)$ for ${}^7\text{Li}$,	9
Melting point, °C	1545	9

2.2 Thermal properties

Item	Data	Refs.
Vapor pressure	Temperature at which total lithium vapor pressure is 0.01 Pa , K $839 + (305 + 87.3 \log 100 P(\text{D}_2\text{O})) - 78.3 \log P(\text{D}_2) /$ $[1 + 2.55 \times 10^{-10} \log 100 P(\text{D}_2\text{O})^{18.6}]$ $10 \leq P(\text{D}_2) \leq 1000 \text{ Pa}$, $0.01 \leq P(\text{D}_2\text{O}) \leq 100 \text{ Pa}$	13 14 15 16
Specific heat, kJ / kg-K	$355 (T - 100)^{1.1} / (1 + 0.3 T^{1.05})$ $300 \leq T \leq 1400 \text{ K}$	****
Thermal conductivity, W/m-K	$(1 - \epsilon)^{2.9} (5.35 - 4.78 \times 10^{-3} T + 2.87 \times 10^{-6} T^2)$ $0.14 \leq \epsilon (\text{porosity}) \leq 0.25$, $400 \leq T \leq 1400 \text{ K}$	9, 21, 6, 20
Pebble bed thermal conductivity, W/m-K	$(1 - \epsilon) [0.74 + 0.00015 (T - 273) + 3.3 \times 10^{-7} (T - 273)^2] / 0.52$ $0.7 \sim 1.2 \text{ mm diameter pebble}$, 0.1 MPa He $0.43 \leq \epsilon (\text{smear porosity}) \leq 0.48$,	22

300 ≤ T ≤ 1300 K		
Thermal expansion		
Linear expansion, % from 293 K	$\Delta L/L_0 = -0.4119 + 1.154 \times 10^{-3}T + 5.505 \times 10^{-7}T^2$	6
Instantaneous coef. 1/K	$\alpha = 1.154 \times 10^{-5} + 1.101 \times 10^{-8}T$	
Mean coef. from 293K, 1/k	$\alpha_m = (-0.004119 + 1.154 \times 10^{-5}T + 5.505 \times 10^{-9}T^2) / (T - 293)$ 373 ≤ T ≤ 1073 K	

**** : 9, 17, 18, 19, 6, 20

3. Li₂ZrO₃

3.1 Physical properties

Item	Data	Refs.
Molecular weight, g/g-mol	153.25 (1 - 1.31 × 10 ⁻² δ), δ = ⁶ Li fraction in Li	9
Crystalline structure	Monoclinic	9
Density, g/cm ³	4.1573 (1 - 1.31 × 10 ⁻² δ)	9
Li density, g/cm ³	0.3264 δ for ⁶ Li, 0.3807 (1 - δ) for ⁷ Li,	9
Melting point, °C	1695 ± 15	24,24

3.2 Thermal properties

Item	Data	Refs.
Vapor pressure, Pa	$\log P(\text{Li}) = -18.39 \times 10^3 / T + 10.69$ 1031.. ≤ T ≤ 1642 K	25
Specific heat, kJ /kg-K	$C_p = 1.022 - 3.696 \times 10^{-5}T - 2.791 \times 10^{-4}T^{-2}$ 350 ≤ T ≤ 1012 K	26
Thermal conductivity, W/m-K	$k = (1 - \epsilon)^{5/3} [3.643 (1 + 1.549 \times 10^{-3}T)^{-1} + 7.579 \times 10^{-10}T^3]$ 0.187 ≤ ε (porosity) ≤ 0.211, 373 ≤ T ≤ 1063 K	27
Thermal expansion		22
Linear expansion, %	$\Delta L/L_0 = 9.89 \times 10^{-4} (1 + 1.13 \times 10^{-5}T)(T - 298)$	
Instantaneous coef. 1/K	$\alpha = 9.86 \times 10^{-6} (1 + 2.27 \times 10^{-5}T)$	
Mean coef. 1/K	$\alpha_m = 9.89 \times 10^{-6} (1 + 1.13 \times 10^{-5}T)$	

4. α Li₄SiO₄

4.1 Physical properties

Item	Data	Refs.
Molecular weight, g/g-mol	120.126 (1 - 3.315 × 10 ⁻² δ), δ = ⁶ Li fraction in Li	9
Crystalline structure	Monoclinic	9
Density, g / cm ³	2.3993 (1 - 3.332 × 10 ⁻² δ)	10
Li density, g / cm ³	0.4805 δ for ⁶ Li, 0.5604 (1 - δ) for ⁷ Li,	10
Melting point, °C	1255	9

4.2 Thermal properties

Item	Data	Refs.
Vapor pressure, Pa	$\log P(\text{Li}) = 14.948 - 23602 / T$ $\log P(\text{O}_2) = 14.769 - 24473 / T$ $\log P(\text{Li}_2\text{O}) = 21.651 - 36223 / T$ 1385 ≤ T ≤ 1516 K $\log P(\text{LiOH}) = 8.686 - 11580 / T$ at P(H ₂ O) = 10.1 Pa	29 30
Specific heat, kJ / kg-K	$C_p = 0.890 + 1.46 \times 10^{-3}T + 4.01 \times 10^{-5}T^2$ 272 ≤ T ≤ 873 K	9,10 28

Thermal conductivity, W/m-K	$k = (1 - \epsilon)^{5/3} (2.49) [(1 + 2.06 \times 10^{-3} T)^{-1} + 1.85 \times 10^{-10} T^3]$ $0.16 \leq \epsilon$ (porosity) ≤ 0.30 , $373 \leq T \leq 873$ K	31 32
Thermal expansion Linear expansion, % Instantaneous coef. 1/K Mean coef. 1/K	$\Delta L/L_0 = 1.267 \times 10^{-3} (1 + 1.065 \times 10^{-3} T)(T - 298)$ $\alpha = 8.669 \times 10^{-6} (1 + 1.312 \times 10^{-3} T)$ $\alpha_m = 121.67 \times 10^{-6} (1 + 1.065 \times 10^{-3} T)$ $298 \leq T \leq 1273$ K	33

Table A-2 Mechanical properties of candidate breeder materials

1. Li_2O

Item	Data	Refs.
Young's modulus, GPa	$E = 141 \exp(-3.5 p) [1 - 2.3 \times 10^{-4} (T - 293)]$ $0.07 \leq p \leq 0.20$, $T = 293$ K	34
Poisson's ratio	$\nu = 0.19$ (93% dense pellet), $T = 293$ K $= 0.16$ (single crystal), $298 \leq T \leq 1603$ K	35
Ultimate compressive strength, MPa	$\sigma_c = 800 \text{ dg}^{-0.5} \exp(-10 p) \cdot (2000/T)$ dg = grain diameter in μm .	34
Ultimate bending strength, MPa	$\sigma_b = 195 \text{ dg}^{-0.5} \exp(-4.3 p) \cdot (2000/T)$ dg = $10 \mu\text{m}$, $p = 0.2$, $T = 293$ K	34
Tensile failure strength, MPa	$\sigma_a = 195 \text{ dg}^{-0.5} \exp(-4.3 p) \cdot (2000/T)$ dg = $10 \mu\text{m}$, $p = 0.2$, $T = 293$ K	34
Thermal creep rate, 1/s	$\epsilon_c = 8.8 \times 10^2 (1 - p^{2/3})^{-n} \exp(-4.04 \times 10^4/T) \sigma^n$ $n = 5.9$ for $T < 973$ K $n = 5.9 [1 - 1.1 \times 10^{-3} (T - 973)]$, $973 \leq T \leq 1123$ K $n = 4.9$ for $T > 1123$ K $0.07 \leq p \leq 0.21$, $973 \leq T \leq 1223$ K, $4 \leq \sigma \leq 45$ MPa	34

2. $\beta\text{Li}_2\text{TiO}_3$

Item	Data	Refs.
Young's modulus, GPa	$266.8 (1 - \epsilon)(1 - 1.2 \epsilon)^2$ $0.1 \leq \epsilon$ (porosity) ≤ 0.3 , 300 K, 1~2 μm grains	6
Poisson's ratio	$0.3(1 - \epsilon)$, $0.1 \leq \epsilon$ (porosity) ≤ 0.3 , 300 K	6
Rupture strength, MPa	$170(1 - 2.27 \epsilon)$, $0.1 \leq \epsilon$ (porosity) ≤ 0.3 , 300 K, 1~2 μm grains size	36
Bending strength, MPa	60, 300 K, 85% T.D. 10 μm grains size	36
Pebble crush strength, N	30 Weibull (4~10 μm grains, 85% dense, 1.2 mm) 40 Weibull (40~140 μm grains, 78% dense, 1.2 mm) 40 Mean (~20 μm grains, 67% dense, 1.6 mm)	22 37
Vickers hardness, MPa	$363(1 - 2.36 \epsilon)$, $0.1 \leq \epsilon \leq 0.3$, 300 K,	6
Thermal creep rate, 1/s	No data	

3. Li_2ZrO_3

Item	Data	Refs.
Young's modulus, GPa	$E = 203.5 (1 - p)(1 - 1.286 p)^2 [1 - 2.40 \times 10^{-4} (T - 293)]$ $T = 293$ K, $p = \text{porosity}$	38

Poisson's ratio	$\nu = 0.2$	39
Ultimate compressive strength, MPa	$\sigma_c = 396$, dg (grain diameter in μm) = $0.8 \mu\text{m}$, 80 % T.D. $\sigma_c = 230 \pm 31$, $dg = 2 \mu\text{m}$, 80 % T.D.	38 26
Ultimate bending strength, MPa	$\sigma_b = 65 \pm 15$ (25 °C), 60 ± 20 (400 °C), 63 ± 1 (600 °C) $dg = 2 \mu\text{m}$, 80 % T.D.	26
Vickers hardness, MPa	$504.6 (1 - 2.36 \epsilon)$, $\epsilon = \text{porosity}$, 263.4 (80 % T.D.)	6
Thermal creep rate, 1/s	2×10^{-6} (26 MPa), 8×10^{-6} (745 MPa), 4×10^{-5} (144 MPa) at 900 °C	40

4. $\alpha \text{Li}_4\text{SiO}_4$

Item	Data	Refs.
Young's modulus, GPa	$E = 110 (1 - p)^3 [1 - 2.5 \times 10^{-4} (T - 293)]$ $0.02 \leq p$ (porosity) ≤ 0.32 , 293 K,	41 42
Poisson's ratio	$\nu = 0.24$, $p = 0.1$, $T = 293$ K	42
Ultimate compressive strength, MPa	$\sigma_c = 975 dg^{-0.44} (1 - p)^{1.5}$, $15 \leq dg \leq 100 \mu\text{m}$ $0.06 \leq p \leq 0.28$, 293 K, ($dg = \text{grain diameter in } \mu\text{m}$)	42
Ultimate bending strength, MPa	$\sigma_b = 275 dg^{-0.5} \exp(-4.3 p)$, $4 \leq dg \leq 50 \mu\text{m}$ $0.02 \leq p \leq 0.32$, $T = 293$ K	41
Tensile failure strength, MPa	$\sigma_{ft} = 150 dg^{-0.5} \exp(-4.3 p) \cdot (1850/T)$ $4 \leq dg \leq 50 \mu\text{m}$, $0.02 \leq p \leq 0.32$, $T = 293$ K	34
Thermal creep rate, 1/s	$\epsilon_c = 1.4 \times 10^{-2} \exp(-2.5 \times 10^3/T) \sigma$ $10 \leq \sigma \leq 40$ MPa, $0.08 \leq p \leq 0.22$, $1000 \leq T \leq 1220$ K	42

Table A-3 Chemical stability and compatibility (interaction with other materials)

1. Li_2O

Item	Data	Refs.
Hydrogen Solubility in Li_2O , (H) ppm (Li_2O)	$S_H = 7.1 \exp(-2000/T) P(\text{H}_2)^{0.5}$ $20 \leq P(\text{H}_2) \leq 200$ Pa, $476 \leq T \leq 963$ K	43
Interaction with Water Liquid	$\text{Li}_2\text{O} + \text{H}_2\text{O} \rightarrow 2 \text{LiOH} + 125 \text{ kJ/mole LiOH}$	9
Water Vapor Solubility, (OH) ppm (Li_2O)	$S_H = 10^{-A} [9.864 \times 10^{-6} P(\text{H}_2\text{O})]^B$ $A = 23.667 - 2.502 \times 10^{-2} T + 9.62 \times 10^{-6} T^2$ $B = 0.427 + 1.7 \times 10^{-4} T$ $2 \leq P(\text{H}_2\text{O}) \leq 2000$ Pa, $713 \leq T \leq 1123$ K	44
Interaction with 316 S.S. (wastaage), mm	$d = 1.06 \times 10^3 \exp(-5920/T) t^{0.5}$ $773 \leq T \leq 1073$ K, $100 \leq t \leq 5600$ h	45,46 47
Interaction with Be	No data	

2. $\beta \text{Li}_2\text{TiO}_3$

Item	Data	Refs.
Hydrogen Solubility,	$\leq 3 \times 10^{-7} \exp(3600/T) \text{ mol fr. / Pa}^{0.5}$ $73 \leq T \leq 773$ K, $2 \sim 100$ Pa	22
Hydrogen Adsorption	No data	
Interaction with Water	Low solubility in water $\ll 1\%$ uptake after 6 month exposure to room air	6
Interaction with Be	No data	

Interaction with 316 S.S. penetration depth, μm	$3600 t^{0.5} \exp(-9000/T)$ 0.1 MPa He, $823 \leq T \leq 923 \text{ K}$, $410 \leq t \leq 1023 \text{ h}$	21
Interaction with Acids, Li dissolution	90 % after 4 hrs in 95 % aqua-regia+5 % HF 84 % after 15 hrs in 1 M HNO_3 at 323 K	6,21 22,48

3. Li_2ZrO_3

Item	Data	Refs.
Hydrogen Solubility	No data	
Hydrogen Adsorption	No data	
Interaction with Water Liquid	Hydrolyses at 25 °C and 100 °C	26,44 38
Water Vapor Solubility	No data	
Water Vapor Adsorption	No data	
Interaction with Steels	No significant interaction in conditions explored: up to 700 °C in vacuum	45
Interaction with Be	No significant interaction up to 650 °C in vacuum slight oxidation of beryllium in wet helium	50

4. $\alpha\text{-Li}_4\text{SiO}_4$

Item	Data	Refs.
Hydrogen Solubility, (H) ppm (Li_4SiO_4)	No data	
Interaction with Water Liquid	No data	
Water Vapor Solubility, (OH) ppm (Li_4SiO_4)	No data	
Water Vapor Adsorption, mols (OH) / m^3	No data	
Interaction with Steels, Dry, penetration depth, mm	$d^2 = 1 \times 10^5 t \exp(-1.20 \times 10^4 / T)$ $25 \leq t \leq 500 \text{ h}$, $973 \leq T \leq 1273 \text{ K}$	45
Interaction with Steels, P (H_2O) at 10 Pa penetration depth, mm	$d^2 = 2.5 \times 10^5 t \exp(-1.20 \times 10^4 / T)$ $25 \leq t \leq 500 \text{ h}$, $973 \leq T \leq 1273 \text{ K}$	51
Interaction with Be, penetration depth, mm	$d^2 = 1.1 \times 10^5 t \exp(-1.02 \times 10^4 / T)$ $100 \leq t \leq 1000 \text{ h}$, $923 \leq T \leq 1023 \text{ K}$	52

Table A-4 Irradiation effects and miscellaneous effects of candidate breeder materials

1. Li_2O

1.1 Irradiation effects

Item	Data	Refs.
Physical integrity	Fair for 500, 700, 900 °C (< 3 at. % ^6Li burn-up) Fair for 550 ~ 1000 °C (4 at. % ^6Li burn-up)	47 53
Swelling	$\Delta V / V_0, \%$ Burn-up at. % 500 °C 700 °C 900 °C 1 -1.0 5.0 6.0 2 -3.5 7.5 6.0 3 -2.8 7.0 6.0	47

Grain growth, μm at 1 at. % ^6Li burn-up	500 °C 3.5 → 3.5	700 °C 3.5 → 7.0	900 °C 3.5 → 17.0	54
Helium retention	Retained / Generated. % Burn-up at. % 500 °C 700 °C 900 °C			55
	1	25	25	10
	2	14	22	5
	3	13	23	7
Li transport, g / h	$W = (29.9 / 2) F [K \cdot P(\text{H}_2\text{O})]^{0.5} / P(\text{total})$ $F = \text{He sweep gas flow rate (mol / h)}$ $K = [P(\text{LiOH})]^2 / P(\text{H}_2\text{O})$, equilibrium constant for $\text{Li}_2\text{O(s)} + \text{H}_2\text{O(g)} \rightarrow 2 \text{LiOH(g)}$ $P(\text{H}_2\text{O}) = \text{water vapor pressure in atm.}$ $P(\text{total}) = \text{total sweep gas pressure, atm.}$			56 57
Thermal conductivity	Slight decrease at low temp. due to fast neutron irradiation			58
Young's modulus	No data			
Compressive strength	No data			
Bending strength	No data			
Tritium diffusivity, cm^2/s	$D = 4.03 \times 10^{-2} \exp[-95.1 (\text{kJ} / \text{mol}) / RT]$ $573 \leq T \leq 1173 \text{ K}$, $R = 8.31 \times 10^{-3} \text{ kJ} / \text{m-K}$ Single crystal diffusivity decreases with irradiation			59
Tritium residence time, h	$\tau = \exp(2.273 \times 10^4 / T - 34.83)$, He + 0.1 % He purge $dg \sim 16 \mu\text{m}$, $p \sim 20\%$, $593 \leq T \leq 773 \text{ K}$,			60

1.2 Miscellaneous effects

Item	Data	Refs.
Effects of thermal cycling on strength	Performed extremely well. Pebble dia. 1 mm, 92 % T.D., 42 μm grain size, 400 – 800 °C heating –cooling rate of 20 °C /s, Up to 2000 cycles.	63

2. $\beta \text{Li}_2\text{TiO}_3$

2.1 Irradiation effects

Item	Data	Refs.
Physical integrity	No data	
Thermal properties	No data	
Mechanical properties	No data	
Swelling	No data	
Helium retention	Retained fraction, % (1 K/min ramp rate) Burn-up, at. % 673 K 773 K 873 K 0.007 78 10 4	61
Tritium diffusivity	No data	
Tritium residence time, h	Roughly similar to Li_2ZrO_3	****
U.S. Class C waste disposal rating	0.2 at 15 MW. yr / m^2 fluence, 10 - yr cooling	62
Afterheat, W / cm^2	0.05 at 15 MW. yr / m^2 , 1 - hr cooling, 85 % dense	62
Tritium release	Tritium release performance is excellent and is similar to Li_2ZrO_3 . More than 80 % tritium released within ~ 11 hr. at 250 °C (see Fig. 4-1, 4-2).	6 63 64

****: 6, 21, 60, 61, 63, 64

2.2 Miscellaneous effects

Item	Data						Refs.	
	Sample	Number of thermal cycles						
		0	3	6	9	12	15	
Effects of thermal cycling on strength of Li_2TiO_3 sphere in 1.2 mm size. Compressive strength, N	77.6 % T.D. 4 ~ 10 μm grain size	40.9	44.9	43.1	42.7	42.3	42.7	63
	81.3 % T.D. 40 ~ 140 μm grain size	35.6	4.4	9.8	33.4	32.5	31.1	

Note: 1. Thermal cycle; 273 K \rightarrow 1273 K at 200 K/hr.

2. Li_2TiO_3 pellets behavior is expected to be similar to that of Li_2ZrO_3 pellets and that is excellent under ~ 30000 cycles.

3. Li_2ZrO_3

3.1 Irradiation effects

Item	Data	Refs.
Physical integrity	Very good	40
Swelling	Less than 0.7 %	40
Grain growth	No data	54
Li transport	No data	65
Thermal conductivity	No significant change	26
Thermal expansion	No significant change	26
Young's modulus	~ 30 % increase	26
Compressive strength	Significant decrease, not in agreement with bending strength behavior	26
Bending strength	Scattered values available	26
Helium retained	Very low	55
Tritium diffusivity	No single crystal data	
Tritium residence time, h	$\tau = 1.089 \times 10^{-19} \exp(230.5 \text{ kJ mol}^{-1} / RT)$, $T \geq 583 \text{ K}$, $0.5 \leq dg \leq 1 \mu\text{m}$, $20 \leq p \leq 25 \%$ He + 0.1 % He purge	6 60

3.2 Miscellaneous effects

Item	Data	Refs.
Effects of thermal cycling	Pellet (83 % T.D.), 330 \rightarrow 530 $^\circ\text{C}$, 30 MPa, 1000 cycles	No fractured
	Pebble (80 % T.D., 1 mm in size, 40 μm grain size)	Fractured significantly

4. $\alpha\text{-Li}_4\text{SiO}_4$

4.1 Irradiation effects

Item	Data	Refs.		
Physical integrity	Poor at 500, 700, 900 $^\circ\text{C}$ (< 3 at. % burn-up)	45,53		
Swelling	$\Delta V/V_0, \%$			
	^6Li burn-up	500 $^\circ\text{C}$	700 $^\circ\text{C}$	900 $^\circ\text{C}$
	1	0.3	0.3	0.3
	2	-	1.2	0.6
	3	0.4	2.7	2.0

Grain growth	At ~ 1 at. % ^6Li burn-up, none for 500 °C, 700 °C 1 → 2 μm at 900 °C	54								
Helium retention	At 1 at. % ^6Li burn-up <table border="1" style="margin-left: auto; margin-right: auto;"> <tr> <td>T, °C</td> <td>Retained / Generated, %</td> </tr> <tr> <td>500</td> <td>0.7</td> </tr> <tr> <td>700</td> <td>0.6</td> </tr> <tr> <td>900</td> <td>0.06</td> </tr> </table>	T, °C	Retained / Generated, %	500	0.7	700	0.6	900	0.06	58
T, °C	Retained / Generated, %									
500	0.7									
700	0.6									
900	0.06									
Tritium diffusivity, cm ² /s	No single crystal data $D = 1.37 \times 10^{-7} \exp(-63 \text{ kJ/mol} / RT)$ Based on grain size of polycrystalline samples	66								
Tritium residence time, h	$\tau = 2.24 \times 10^{-7} \exp(-63 \text{ kJ/mol} / RT)$, $d_g \sim 20 \mu\text{m}$, $p \sim 0.08$, $560 \leq T \leq 770 \text{ K}$, He + 0.1 % He purge	67								

4.2 Miscellaneous effects

Item	Data	Refs.
Effects of thermal cycling	Pebble (93 % T.D., 1 mm in size, 40 μm grain size), 400 – 800 °C, 20 °C / s, 50 cycles	Fractured significantly
	Pebble (80 % T.D., 0.4–0.6 mm in size, 40 μm grain size), 400 - 800 °C 20 °C / s, 50 cycles	Good performance
		68

References

- 1) Y.Futamura, K.Horii and H.Kawamura, Ann. Rept. Hydrogen Isot. Res. Ctr. Toyama Univ. 15 (1995)85.
- 2) Y.Futamura and H.Kawamura, Ann. Rept. Hydrogen Isot. Res. Ctr. Toyama Univ. 16(1996)93.
- 3) Y.Futamura, K.Tsuchiya and H.Kawamura, Ann. Rept. Hydrogen Isot. Res. Ctr. Toyama Univ. 17(1997)97
- 4) M.C.Billon, W.Dienst, T.Flament. P.Lorenzette, K.Noda and N.Roux, " ITER Solid Breeder Blanket Materials Database", May 1993, ANL / FPP / TM - 263
- 5) ITER Documentation Series, No. 29, ITER BLANKET, SHIELD AND MATERIAL DATA BASE, IAEA, 1991
- 6) N.Roux, J.Avon, A.Floreancing, J.Mougin, B.Rasneur, S.Ravel, "Low-temperature Tritium Releasing Ceramics as Potential Materials for the ITER Breeding Blanket", Proc. 4th Int. Workshop on Ceramic Breeder Blanket Interactions, Oct.9-11,1995, Kyoto, Japan,
- 7) P.Gierzewski, "Review of Properties of Lithium Metatitanate", CFFTP G-9561, Oct. 1995.
- 8) P.Gierzewski, "Review of Properties of Lithium Metatitanate", CFFTP G-9703, Oct, 1997
- 9) D.J.Suiter, "Lithium Based Ceramics for tritium Breeding Applications," McDonnel Douglas Astronautics Company Report MDC E2677 (UC-20), June 1983.
- 10) J.W. Davis, "Materials Handbook for Fusion Energy Systems," U.S.Department of Energy Report, DOE/TIC-10122 (1980 – 1986).
- 11) H.Kudo, C.H. Wu and H.R. Ihle, "Mass-spectrometric Study of the Vaporization of $\text{Li}_2\text{O}(\text{s})$ and Thermochemistry of Gaseous LiO , Li_2O , Li_3O , and Li_2O_2 ," J.Nucl. Mater. 78 (1987) 380.
- 12) T.Takahashi and T.Kikuchi, "Porosity Dependence on Thermal Diffusivity and Thermal Conductivity of Li_2O from 200 to 900 °C," J. Nucl. Mater. 91(1980) 93.
- 13) J.P.Kopasz and C.E.Johnson, "Investigation of the interaction of $\text{H}_2\text{O}(\text{g})$ with Li_2ZrO_3 ", Proc.4th Inter. Workshop on Ceramic Breeder Blanket Interactions, Kyoto(1995) 224.
- 14) M.Asano, Y.Kato, T.Harada and Y.Mizutani, "Vaporization and thermochemical properties of lithium containing complex oxides ", Proc. 4th Inter. Workshop on Ceramic Breeder Blanket Interactions, kyoto(1995)259.
- 15) M.Yamawaki, A.Suzuki, M.Yasumoto and K.Yamaguchi, "Investigations on the interactuons $\text{D}_2\text{O}(\text{g})$ and $\text{D}_2(\text{g})$ with Li_2TiO_3 and other ceramic breeders by means

- of atmosphere controlled HT mass spectrometer", Proc. 5th Inter. Workshop on Ceramic Breeder Blanket Interactions , Rome(1996).
- 16) H.Nakagawa, M.Asano and K.Kubo, "Mass spectrometric investigation of the vaporization of $\text{Li}_2\text{TiO}_3(\text{g})$," J. Nucl. Mater. 110(1982)158.
 - 17) I.Barin and O.Knake, "Thermochemical properties of inorganic substances", Springer Verlag (1973)425
 - 18) "JANAF Thermochemical Tables", US Nat. Bur. Standards (1964).
 - 19) A.Christensen, K.C.Conway et al., "High temperature heat content and entropies of aluminates and ferrites of lithium, sodium, and lithium titanate", US Bur. Mines Report RI-5565(1960)
 - 20) J.Davis and A.Haasz, "Thermal diffusivity / conductivity of AECL Li_2TiO_3 ceramic", J. Nucl. Mater. 232 (1996) 65.
 - 21) P.Finn, T.Kurasawa, S.Nasu, K.Noda and H.Watanabe, "Solid oxide compounds properties necessary for fusion applications", Proc. IEEE 9th Symp. On Eng. Problems of Fusion Research (Chicago, 1981), Vol. 11, 1200.
 - 22) P.Gierszewski et al, "Canadian ceramic breeder technology: recent results", Fusion Eng. & Design 27 (1995) 297 (Proc. ISFNT-3, Los Angeles, 1994)
 - 23) "Semi-Annual Report of KfK / Euratom April-September 1989", KfK Report 4677, Nov. 1989.
 - 24) G.P.Wyers and E.H.P.Gordfunke, "Phase Relation in the System Li_2ZrO_3 ", J. Nucl. Mater. 168 (1989) 24.
 - 25) A.Neubert and D.Guggi, J. Chem. Thermo. 10(1978) 297- 306.
 - 26) D.A.Moor, " A Compilation of Data and a Review of the properties of Lithium Monoxide and Lithium Zirconates Relevant to Their Use as Tritium Breeder Material in Fusion Reactors", NRL-R-2014 (S) to be published.
 - 27) W.dienst and H.Zimmerman, " Investigation of the Mechanical properties of Ceramic Breeder Materials", J. Nucl. Mater. 155-157 (1988) 476.
 - 28) G.W.Hollenberg, "Thermal Properties of Lithium Ceramics for Fusion Applications", 84th Annual Meeting of American Ceramic Society, Cincinnati, Ohio, May 3-5, 1982.
 - 29) H.R.Ihle, R.D.Penzhorn, and P.Sshuster, "The Thermochemistry of Lithium Silicates in View of Their Use as Breeder Materials ", Fusion Eng. Design 8 (1989) 393.
 - 30) O.Gotzmann, " Thermodynamics of Ceramic Breeder Materials for Fusion Reactors ", J. Nucl. Mater. 167 (1989) 213.
 - 31) Y.Takahashi, 2nd Int. Symp. Fabrication and Properties of Li-Ceramics, Indianapolis, IN, May 3-5, 1982.
 - 32) B.Schultz, KfK Report 4677 (1989) p.57.

- 33) A.Skokan, H.Wedemeyer, D.Vllath and F.Guenther, " Thermal Properties and Application of potential lithium silicate Breeder Materials" , Fusion Technology 2 (1986) 1255.
- 34) M.C.Billone and W.t.Grayhack, " Summary of Mechanical Properties Data and Correlations for Li_2O , Li_4SiO_4 , LiAlO_2 , and Be " , Argonne National Laboratory Report ANL/ FPP / TM-218, April 1990.
- 35) S.Hull et al., " The Elastic Properties of Lithium Oxide and Their Variation with Temperature " , J. Nucl. Mater. 160 (1988) 125.
- 36) K. Tsuchiya, K. Watarumi, S. Saito et al, " Fabrication Development of ceramic tritium breeders by sol-gel method " , Proc. 5th International Workshop on Ceramic Breeder Blanket Interactions, Rome (1996) 191.
- 37) H.Hamilton, " The thermal cycling behavior of lithium titanate " , J. Nucl. Mater. 219(1995) 274.
- 38) B.Rasneur, " Fabrication, Mechanical and Chemical Properties of LiAlO_2 and Li_2ZrO_3 as Tritium Breeders for a Solid Blanket" , presented at the 91st Annual Meeting of the American Ceramic Society, Indianapolis, April 1989.
- 39) P.Kennedy, " The Preparation, Characterization and Properties of Lithium Oxide and Metazirconate Specimens Irradiated in HFR Petten in the 2nd and 3rd EXOTIC Experiments" , 14th SOFT, Fusion Technology (1986) 1013.
- 40) W.Dienst, " Contribution of the Data Base for the International Fusion Materials Handbook: Mechanical Properties and Compatibility of Ceramic Breeding Materials" , IMF-Notiz 129 (1989).
- 41) K.Bar, C.Y.Chu, J.P.Singh, K.C.Goretta, J.L.Routbort, M.C.Billone, and R.B.Poeppel, " Mechanical Properties of Polycrystalline Lithium Ortho-silicate" , Fusion Eng. Design 8 (1989) 371.
- 42) H.Zimmermann, " Mechanische Eigenschaften von Lithiumsilikaten für Fusion-Reaktor-Brutblankets" , KfK 4528 (1989).
- 43) H.Kudo, S.O'hira, M.Fujie, and K.Noda, " Interaction of Tritium Gas with Li_2O Crystals and Dissolution Processes" , J. Nucl. Mater. (1991) 880.
- 44) M.Tetenbaum, A.K.Fischer, and C.E.Johnson, " An Investigation of the Solubility of LiOH in Solid Li_2O " , Fusion Techn. 7 (1985) 53.
- 45) P.Hofmann and W.Dienst, "Chemical Compatibility between Lithium-based Oxide Ceramics and Stainless Steels" , J. Nucl. Mater. 141-143 (1986) 289
- 46) O.K.Chopra and D.L.Smith, Oak Ridge National Laboratory Report, DOE/ER-0045/8 (1982) 507-513.
- 47) G.W.Hollenberg, "Pellet Integrity and Swelling of Lithium Ceramics" , in Fusion Reactor Materials Semi-annual Progress Report for Period Ending September 30, 1986, DOE/ER-0313/1 (June 1989) 373-380.

- 48) K.Tsuchiya, H.Kawamura and T.Takeuchi, "Dissolving and recovering properties for reprocessing technology of lithium titanate", 4th International Symposium on Fusion Nuclear Technology, Kyoto(1997).
- 49) B.Rasneur, "Determination of Chemical Characteristics of LiAlO_2 and Li_2ZrO_3 for a Fusion Reactor Blanket", 15th SOFT, Fusion Techn. (1988).
- 50) A.Terlain, D.Herpin, P.Perodeaud, T.Flament and J.Sanier, "Compatibility Problems with Beryllium in Ceramic Blankets", 15th SOFT, Fusion Technology (1988) 1179.
- 51) P.Hofmann and W.Dienst, "Compatibility Studies of Metallic Materials with Lithium-Based Oxides", J. Nucl. Mater. 155-157 (1988) 485.
- 52) P.hofmann and W.Dienst, "Compatibility Interactions of Be with Li-Based Oxides and Stainless Steel," J. Nucl. Mater. 171 (1990) 203.
- 53) O.D.Slagle, G.W.Hollenberg and D.L.Baldwin, "The FUBR-1B Irradiation Experiment -Tritium Release and Physical Stability of Solid Breeder Materials", J. Nucl. Mater., 179-181 (1991) 843.
- 54) G.W.Hollenberg, "Fast Neutron Irradiation Results on Li_2 , Li_4SiO_4 , Li_2ZrO_3 , and LiAlO_2 ," J. Nucl. Mater., 123(1984) 896.
- 55) D.L.Baldwin and G.W.hollenberg, "Measurement of Tritium and Helium in Fast Neutron Irradiated Ceramics Using High Temperature Vacuum Extraction," J. Nucl. Mater., 141-143 (1986) 305.
- 56) O.D.Slagle and G.W.Hollenberg, Proc. 2nd Int. Specialist's Workshop on Modeling Tritium Behavior in Fusion Ceramic Blankets (1989) 181-199.
- 57) T.Kobayashi et al., "Japanese Contributions to IAEA INTOR Workshop, Phase Two A, Part 3," JAERI-M 87-219 (1988).
- 58) J.L.Ethridge, D.E.Baker, A.D.Miller, "Effects of Fast Neutron Irradiation on Thermal conductivity of Li_2O and LiAlO_2 ," J. Am. Ceram. Soc. 71(6)(1988)C-294.
- 59) M.C.Billone, H.Attaya and J.P.Kopasz, "Modeling of Tritium Behavior in Li_2O ," Argonne national Laboratory, ANL/FPP/TM-260, August 1992.
- 60) M.Briec, J.J.Abassin, C.E.Johson, M.Masson, N.Roux and H.Watanabe, "The MOZART Experiment: In-Pile Tritium Extraction from Lithium Oxide Aluminate, Zirconate," Proc. 15th SOFT, Fusion Techn. (1988) 1105.
- 61) J.Mougin, B.Rasneur and N.Roux, "Tritium and helium release from Li_2TiO_3 Comparison with Li_2ZrO_3 ," Proc. 3rd Inter. Workshop on Ceramic Breeder Blanket Interactions, Los Angels (1994).
- 62) M.A.Abdou, A.H.Hadid, A.Rraffray et al, "Modeling, analysis and experiments for fusion nuclear technology," Fusion Eng. Design 6 (1988) 3.
- 63) J.M.miller, H.B.Hamilton and J.D.Sullivan, "Testing of lithium titanate as an alternate blanket material", J. Nucl. Mater. 212-215 (1994) 877-880.

- 64) J.P.Kopasz, J.M.Miller and C.E.Johoson, "Tritium release from lithium titanate, a low activation tritium breeding material", *J. Nucl. Mater.* 212(1994)927.
- 65) Y.Ikeda, H.Ito, G.Matsumoto and H.Hayashi, "The Vaporization and Thermochemical Stability of Lithium Aluminates", *J. Nucl. Mater.* 97 (1981) 47-58.
- 66) M.C.Billone and W.T.Grayhack, "Mechanical Models for Predicting Tritium Trasport in Lithium Ceramics", *Advances in Ceramics, Vol. 25: Fabrication and Properties of Lithium Ceramics* (1989) American Ceramics Society, Inc. pp.15-27.
- 67) M.Kuche, "Material Data Base for the NET Test Blanket Design Studies", April 1989, KfK.
- 68) N.Roux, G.Hollenberg, C.Johnson, K.Noda and R.Verrall, "Summary of experimental results for ceramic breeder materials", *Fusion Eng. Design* 27(1995)154-166.